



## **Acousto-Optic Deflector Driver**

**Including: Basic Deflector Alignment**

### **Instruction Manual**

### **RFA3x0-2**

Models -

RFA340-2 : 10V Tuning Input, 30-50MHz, 10V Analog Modulation Input

RFA350-2 : 10V Tuning Input, 40-60MHz, 10V Analog Modulation Input

#### **Options:**

-BR, brass water cooled heatsink,  
(recommended for low corrosion copper cased AO devices)

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1. GENERAL

The RFA3x0-2 Deflector Driver, figure 1, is a modular, swept-frequency RF power source specifically designed to operate with acousto-optic deflectors. The driver accepts a tuning voltage, typically between approximately +0 volts and +10 volts and provides an RF output to the acousto-optic deflector at the tuned frequency. . The driver also accepts an analogue amplitude modulation signal. This provides for intensity control and/or fast amplitude modulation across the scan range.

A summary of the driver specification is shown in the following table:

| <b>Model</b> | <b>Tuning Range</b><br>(Nominal)** | <b>Modulation</b> | <b>Output Power</b> |
|--------------|------------------------------------|-------------------|---------------------|
| RFA340-2     | 30-50MHz                           | Analog            | 70Watt per channel  |
| RFA350-2     | 40-60MHz                           | Analog            | 70Watt per channel  |

Figure 2 is a block diagram of the Driver. The output frequency of the driver is controlled by a hybridized varactor oscillator circuit. The capacitance of the internal varactor is a function of the applied tuning voltage. The output frequency is proportional to the input tuning voltage with a scale factor of approximately 2.0 MHz/volt. A table of output frequency versus input tuning voltage is supplied with each driver; a typical voltage vs. frequency curve is shown in figure 4. The frequency linearity is typically  $\pm 1.5\%$ , and frequency stability is typically  $\pm 0.25\%$ .

The oscillator output is connected to a matched RF splitter. This provides signal to a diode ring RF modulator and the frequency monitor output. The frequency monitor output provides a low level (approx. 300mVpp) output signal at the tuned operating frequency. This can be used for measurement or feedback purposes.

*\*\* A multi-turn variable potentiometer situated to the right of the front panel LED's allows adjustment of start frequency. This is the frequency output at 0V tuning voltage input.*

*For optimum scan flatness, the operating frequency range may be need to be centered +/- 10% about the nominal centre frequency of 40MHz/50MHz.*

*The limits of this adjustment cover the full tuning range. This allows the driver output frequency to be set at any fixed point across the frequency range.*

A high-frequency, diode ring modulator is used to amplitude-modulate the RF carrier. A 10 volt swing on the modulation input (positive with respect to ground) will result in 100% depth of modulation. Figure 3 shows the modulation control.

The amplitude-modulated RF is applied to a splitter and amplified to a preset level in the two power amp stages. The output amplifiers are designed to operate at full rated power into a 50Ω load with 100% duty cycle. The output power level of both outputs is set by the power adjust potentiometer.

A phase delay is applied between the two RF outputs is defined by an internal delay line.

The delay value is specific to the design of the beam steered deflector.

Typical waveforms are given in Figure 7

### Cooling

Connect cooling water at a flow rate greater than 1 litre/minute, less than 25 deg.C or as required by AO deflector . The driver mounting face temperature must not exceed 70°C.

**Serious damage to the amplifier may also result if the RF output connector is operated open-circuited or short-circuited.**

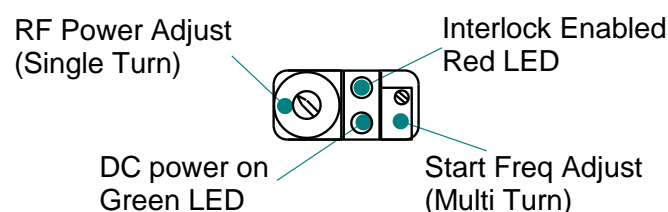
### DC supply

Filtered screw terminal connection.

A low impedance 24Vdc (or 28Vdc) DC power supply is required. The voltage is +24Vdc at a current drain of approximately 9.0A. The external power source should be regulated to ± 2% and the power supply ripple voltage should be less than 200mV for best results.

The driver will output higher RF power if operated from 28Vdc. See test data sheet.

Front panel indicators and adjustments





## 2. SPECIFICATIONS

|   |                                    |
|---|------------------------------------|
| Oscillator Type:                        | Varactor-tuned thin film hybrid    |
| Amplifier Type:                         | Broadband Class A                  |
| Output RF Power:                        | > 70Watt / output (24Vdc)          |
| Output Impedance:                       | 50Ω nominal                        |
| Load VSWR:                              | < 2.5:1 for best results           |
| Output RF Power Variation vs. Frequency | < 1 dB                             |
| Spurious Outputs:                       | Harmonics > 20dB below fundamental |
| Tuning Voltage:                         | 0 to 10V typical                   |
| Tuning Linearity:                       | <1.5% over specified tuning range  |

**DO NOT APPLY NEGATIVE TUNING VOLTAGE  
DO NOT EXCEED + 20V INPUT  
DAMAGE MAY RESULT**

|                           |  |
|---------------------------|--|
| Tuning Voltage Impedance: | ~ 1KΩ  |
| Tuning Slew Rate          | > 10 MHz/μs  |
| Residual FM:              | < 10 KHz peak-to-peak  |
| Frequency Stability:      | ±0.25%   |
| MOD Input Voltage,        | 0-10V for 100% modulation depth                                    |
| MOD Input Impedance:      | ~ 600Ω   |
| RF ON-OFF Ratio:          | > 40 dB  |
| DC Power Input:           | +24Vdc or +28Vdc at <10A regulated to ± 2%                         |
| Temperature Range:        | 0°C to 50°C<br>Mounting face must not exceed 70°C<br>Water cooled. |

## 3. THEORY OF OPERATION

Figures 5 illustrates the key operating parameters. Further explanation is given in the accompanying application notes 'Acousto Optic Deflectors'.



4. INSTALLATION AND ADJUSTMENT (see Figures 1,4,6)
  - a. Connect cooling water at a flow rate greater than 1 litres/minute at less than 25 deg.C
  - b. Connect the + 24Vdc supply. DO NOT APPLY POWER).
  - c. Align the deflector head to insure that the incident light beam is centred in the active aperture of the deflector.
  - d. Connect the two SMA connectors of the deflector to the RF outputs of the RFA3x0-2 beam steered driver. Ensure the coax cables are of equal length. The driver RF outputs must be connected to the AO deflector in an order that depends on the Bragg orientation. Figure 4 illustrates the options. The order of connection is important. The deflector will not be damaged if the order is incorrect but the amplifier outputs must be terminated. If the RF cable connections are incorrect, the deflection efficiency will vary considerably as the deflector frequency is changed.

If required apply a 12V CMOS compatible or open drain connection to the Digital Gate input

- Connect the tuning signal ( 12V tolerant) to pin 7
- Connect the signal return (0V) to pin 2

This input is optional and may be left NC (Not connected).

A closed contact on this input will disable the RF Output. Switching response time 10msec

Connect the external Interlock of the acousto-optic modulator (if fitted) to the enable inputs on the 9-pin D-type connector. If no interlock is fitted then these inputs **MUST** be connected together.

- Connect pin 9 to the floating contact 1 of the interlock switch.
- Connect pin 4 to floating contact 2 of the interlock switch. (Grounded at driver)

- e. Connect the amplitude control source to the D-type connector.

- Connect the modulation signal ( 0,0 - 10.0V) to pin 8
- Connect the signal return (0V) to pin 3

To begin, apply a constant voltage of 10.0V.

- f. Connect the tuning voltage source to the D-type connector .

- Connect the tuning signal ( 0,0 -10.0V) to pin 1
- Connect the signal return (0V) to pin 6

To begin, apply a constant voltage of 5V equivalent to the centre frequency of 40MHz (or 50MHz)



The output frequency can be measured by connecting a frequency counter to the 'Fmon' output connector on the front panel

- g. Start by adjusting the Power adjust potentiometer on the RFA3x0-2 to a fully anti-clockwise direction, (Minimum output). The RF power increases with clockwise rotation of the pot.
- h. Tune the input frequency source to the mid-frequency point of the AO deflector bandwidth
- i. Apply approximately half the required RF power (say 30W / output) at the centre frequency. This is achieved by adjusting the pot ~ 1/3 to 1/2 clockwise from the fully anti-clockwise position. Turn on DC power.

Rotate the deflector slightly until deflection of the light beam occurs. The deflection will occur in the horizontal plane. Select the strongest diffracted spot and monitor the light intensity by using either a photo detector or a light power meter. Re-adjust the Bragg angle for maximum deflected light intensity. Fine tuning of the incident light beam position may be necessary for optimum results.

- j. Adjust RF power level carefully for the desired efficiency at the minimum RF power necessary. Do NOT exceed the RF power level at which maximum efficiency is achieved ( $P_{sat}$ ). Over driving the AO deflector will reduce efficiency and may result in serious damage to the AO crystal.
- k. To equalise deflection efficiency at the extremes of the scan, alternate between the minimum and maximum desired frequencies and adjust Bragg angle to give the same efficiency for both. (Note: the photo detector or light power meter will require repositioning for the two angles.) Sweeping the freq' input should result in a continuous deflected line output. If significant peaks and troughs are noted across the sweep, it is probable that the phase delayed outputs of the RFA3x0-2 are connected to the incorrect inputs of the AO deflector. (see Fig 4)
- m. The lead lengths between the four outputs of the RFA3x0-2 and the beam steered deflector should be equal unless otherwise instructed. Unequal lengths of more than a 1cm would introduce a phase error. Within limits, small changes in the relative lead lengths can be used to fine tune the deflector sweep response, although this is not usually required. The Bragg angle would need re-adjustment.



## 5. THERMAL EFFECTS

We must consider the thermal effects of this device - both due to optical and acoustic absorption. The majority of heat is generated by RF drive power. As the temperature of the material increases beyond the recommended level, undesired refractive index changes will occur in the material. This results in beam distortion. Ultimately, the crystal will crack due to thermal stresses, if excessive RF power is applied.

## 6. MAINTENANCE

### 6.1 Cleaning

It is of utmost importance that the optical apertures of the deflector optical head be kept clean and free of contamination. When the device is not in use, the apertures may be protected by a covering of masking tape. When in use, frequently clean the apertures with a pressurized jet of filtered, dry air.

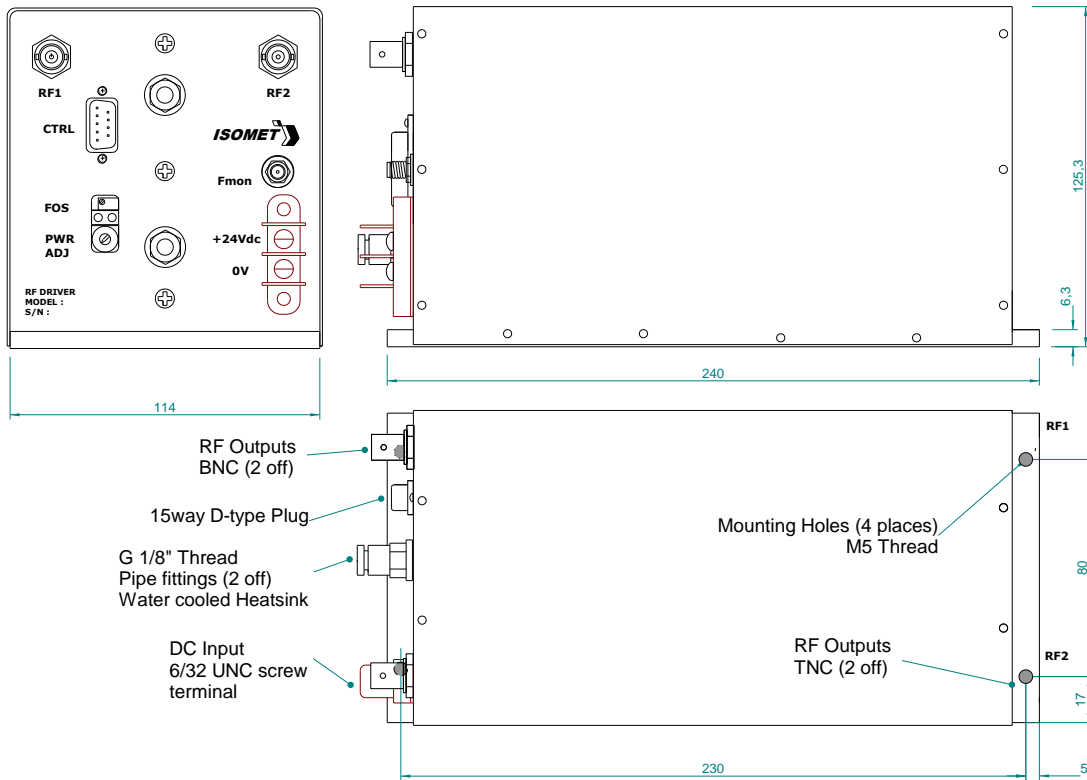
It will probably be necessary in time to wipe the coated window surfaces of atmospherically deposited films. Although the coatings are hard and durable, care must be taken to avoid gouging of the surface and residue of the cleaning solution. It is suggested that the coatings be wiped with a soft ball of brushed (short fibres removed) cotton, slightly moistened with clean alcohol. Before the alcohol has had time to dry on the surface, wipe again with dry cotton in a smooth, continuous stroke. Examine the surface for residue and, if necessary, repeat the cleaning.

### 6.2 Troubleshooting

No troubleshooting procedures are proposed other than a check of alignment and operating procedure. If difficulties arise, take note of the symptoms and contact the manufacturer.

### 6.3 Repairs

In the event of deflector malfunction, discontinue operation and immediately contact the manufacturer or his representative. Due to the high sensitive of tuning procedures and the possible damage, which may result, no user repairs are allowed. Evidence that an attempt has been made to open the optical head will void the manufacturer's warranty.



|                                     |   |                    |
|-------------------------------------|---|--------------------|
| Control signals -                   | : | 9 pin 'D' type     |
| Tuning Voltage                      | : | +sig pn1, -rtn pn6 |
| Amplitude Control                   | : | +sig pn8, -rtn pn3 |
| Enable/Interlock Control (Low = On) | : | +sig pn9, -rtn pn4 |
| Digital Gate Input(NC or High = On) | : | +sig pn7, -sig pn2 |

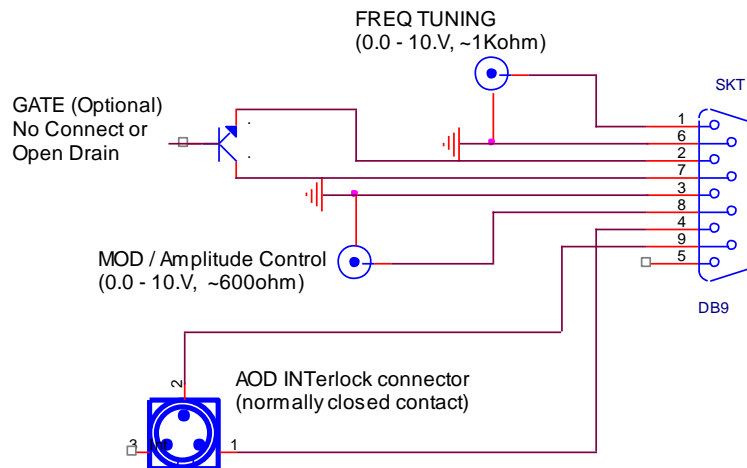


Figure 1:



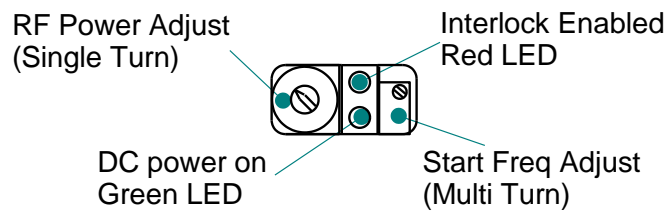
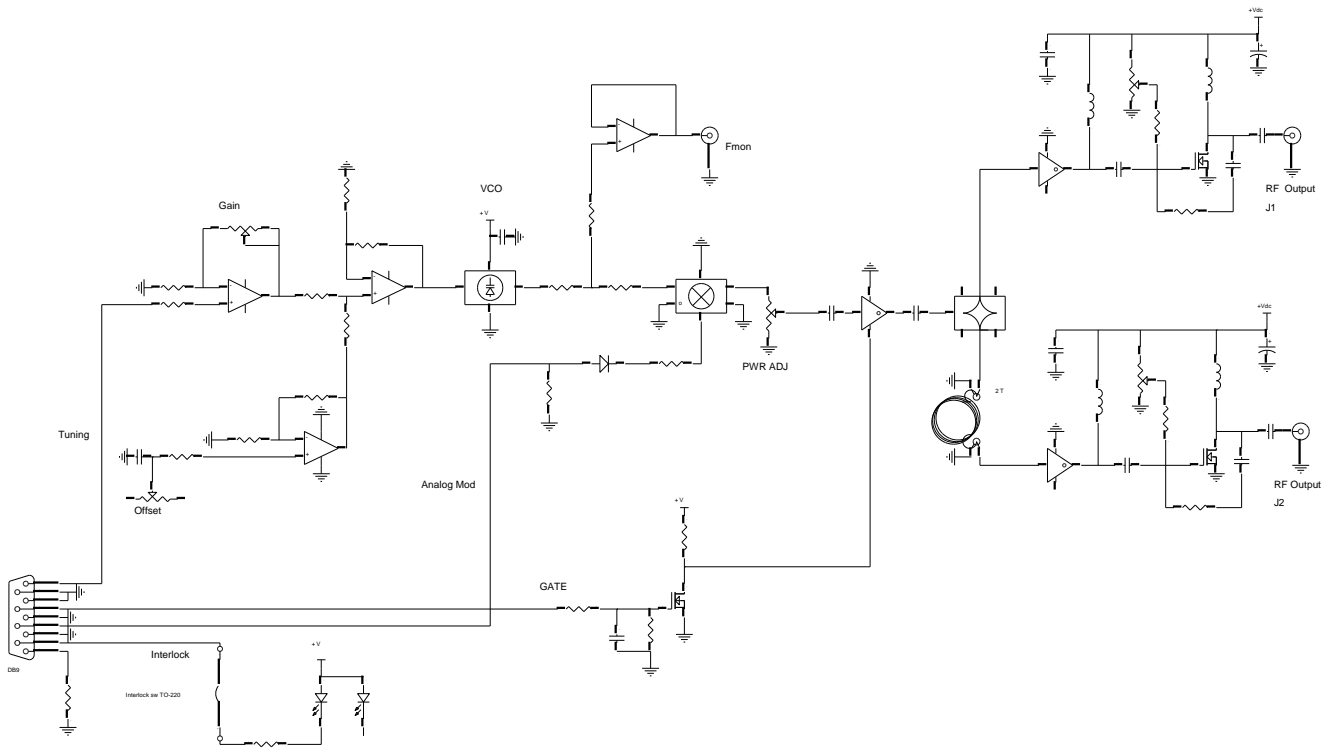
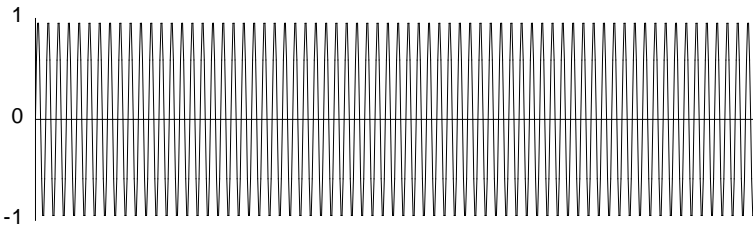
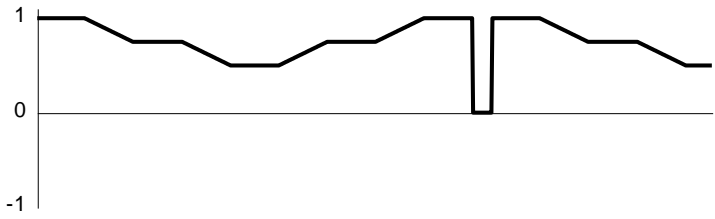


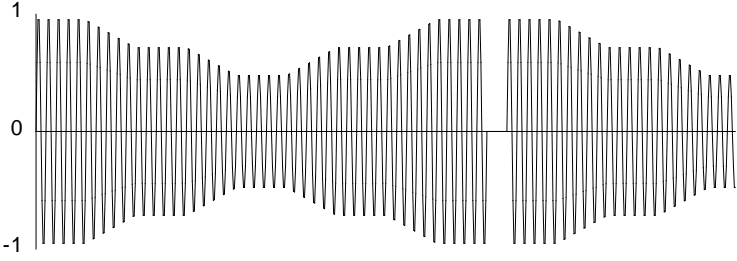
Figure 2, Driver Block Diagram



RF Carrier (FRQ input)

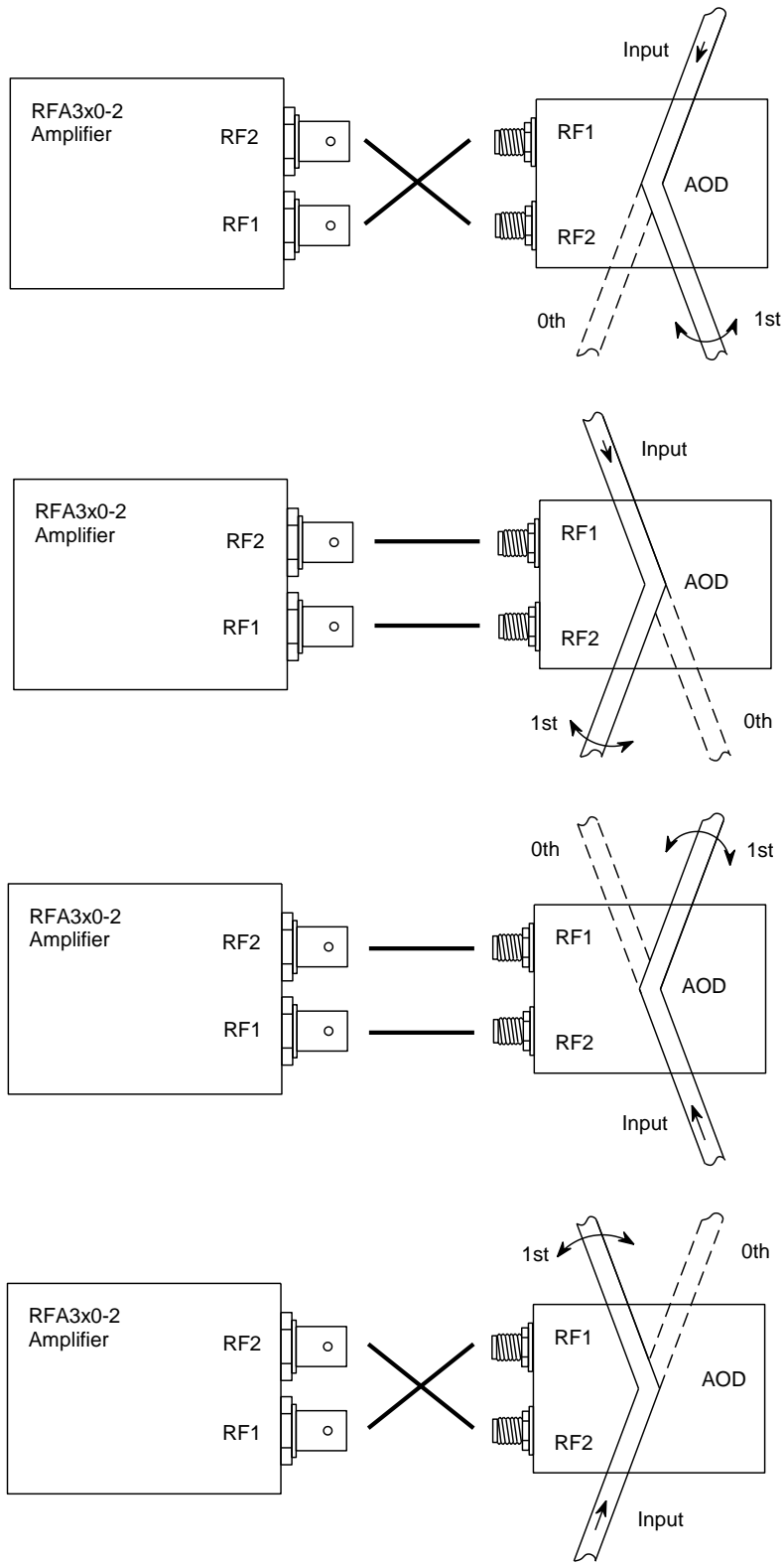


MOD Input



Modulated RF

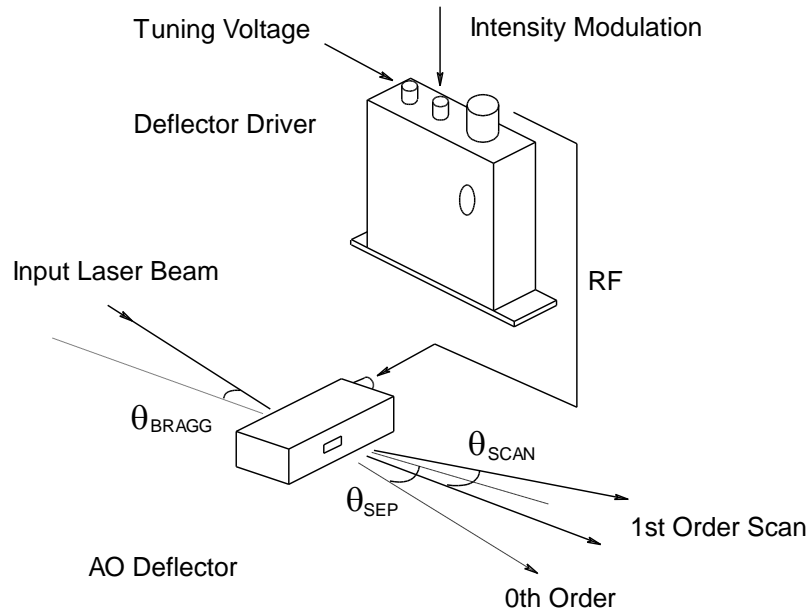
Figure 3, Typical Amplitude Modulation Waveforms



Correct orientation as viewed from top of AOD  
(Connector identification may differ)

Figure 4

**Schematic of a single electrode acousto optic deflector and tunable driver**



The input bragg angle, relative to a normal to the optical surface and in the plane of deflection is given by:

$$\theta_{BRAGG} = \frac{\lambda \cdot fc}{2 \cdot v}$$

The separation angle between the zeroth order and mid scan point of the first order is given by:

$$\theta_{SEP} = \frac{\lambda \cdot fc}{v}$$

The first order scan angle is given by:

$$\theta_{SCAN} = \frac{\lambda \cdot \delta f}{v}$$

The access time or time aperture is given by:

$$T_{acc} = d/v$$

- where :
- $\lambda$  = wavelength
  - $\delta f$  = scan frequency bandwidth
  - $fc$  = centre frequency
  - $v$  = acoustic velocity of the crystal material (Ge = 5.5mm/usec)
  - $d$  = beam diameter

Figure 5, Deflector parameters

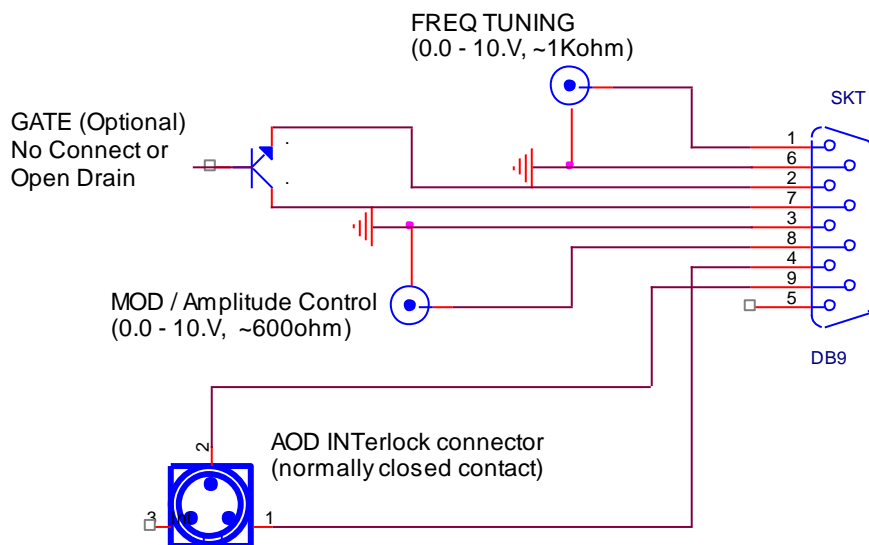
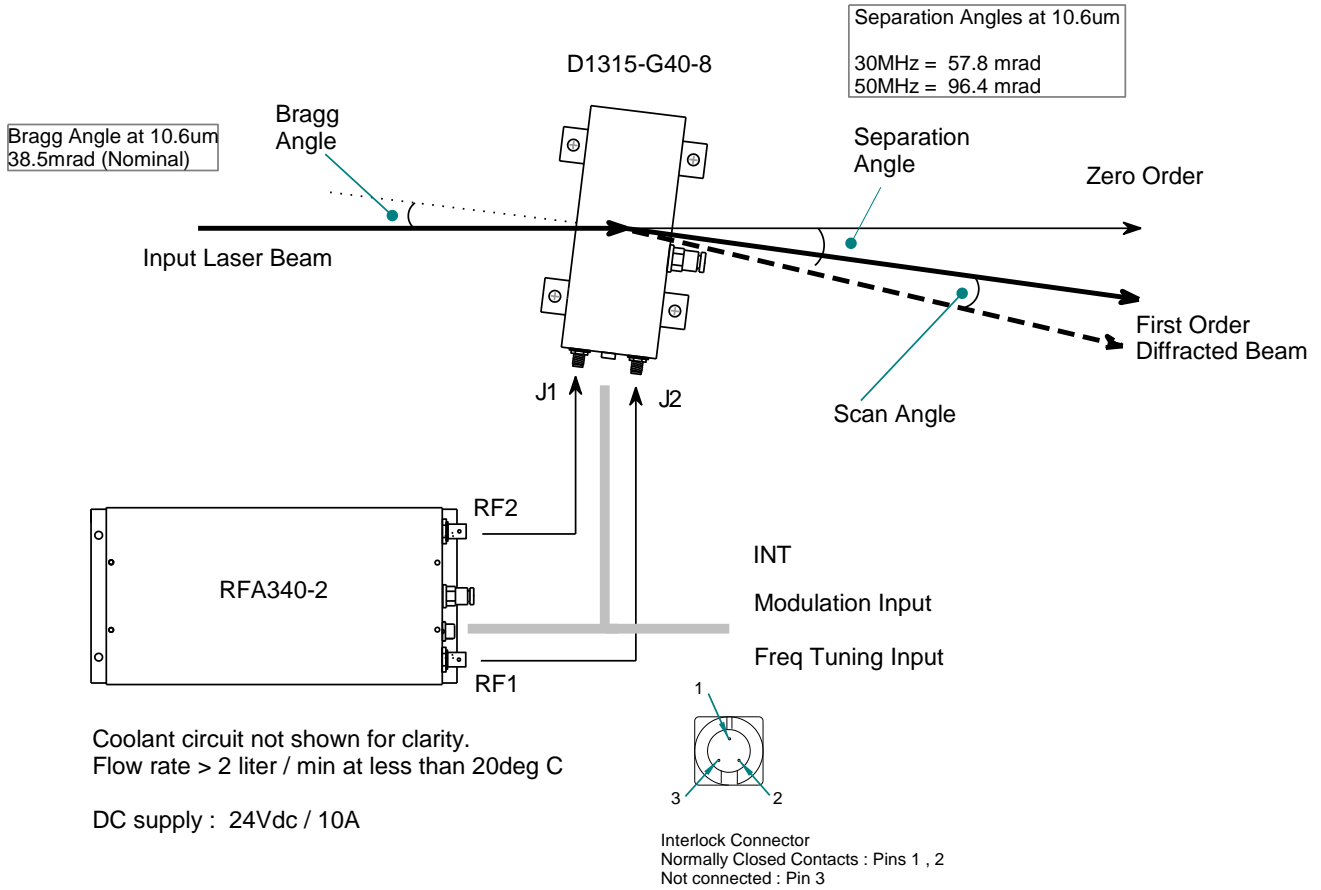
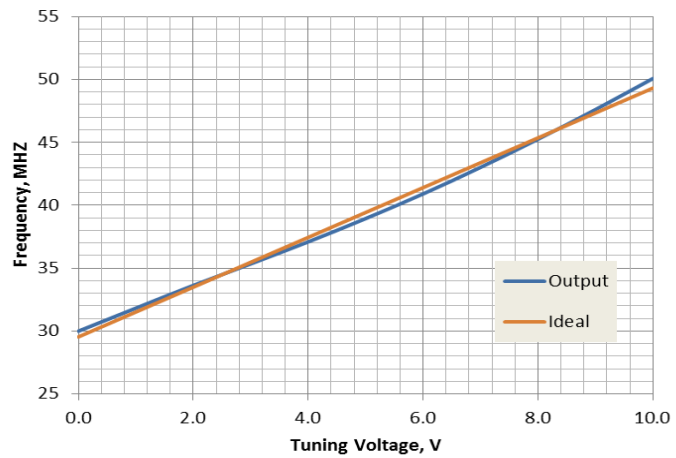


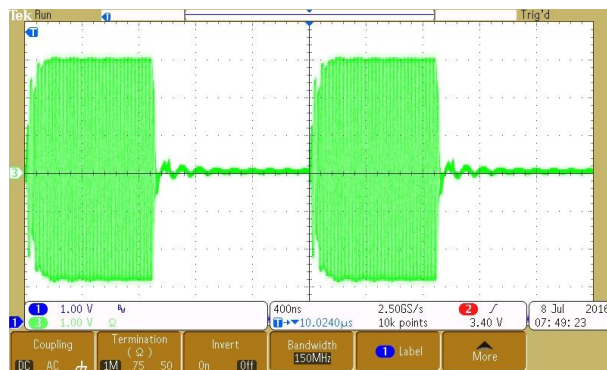
Figure 6. Typical orientation

Typical Tuning Characteristic



Typical Modulation Characteristic

500kHz at 60W / 40MHz RF  
(per output)



Typical RF Power vs. Frequency response (1dB/div)

30-50MHz sweep.

20W, 40W and 80W  
nominal RF power settings

(per output)



Figure 7